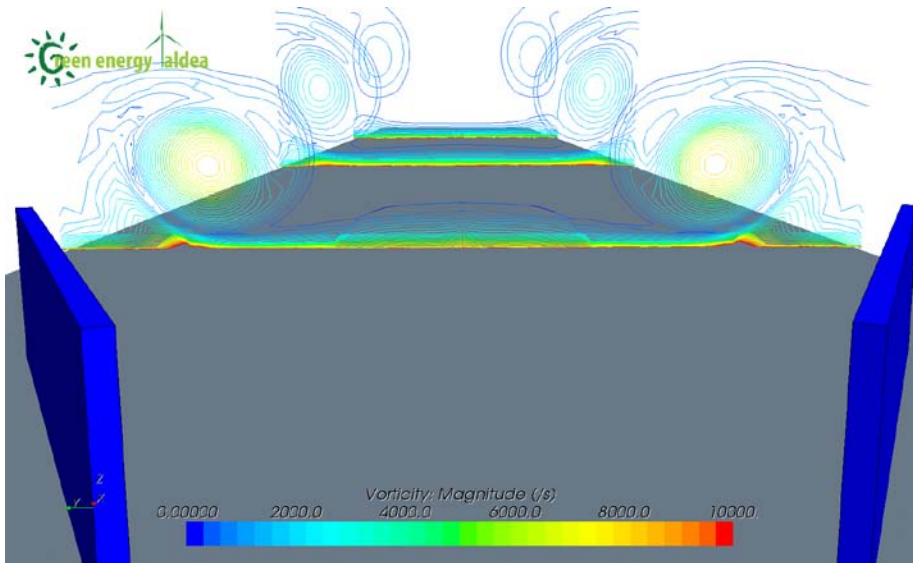




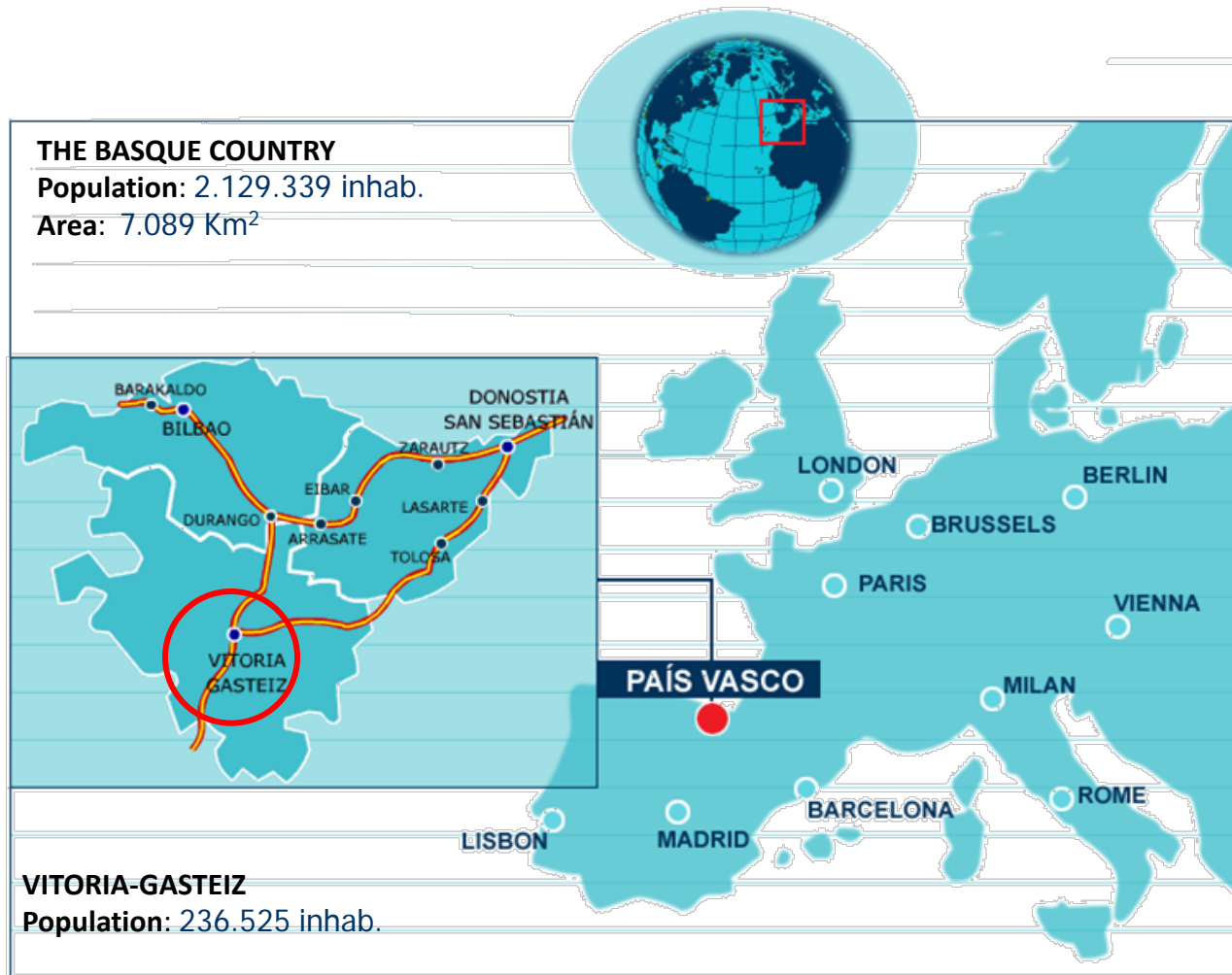
# Computational Simulations of a pair of Rectangular Vortex Generators on a flat plate.



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U. Fernández\*,  
A. Peña,  
K. Olalde.

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# UNIVERSITY LOCATION



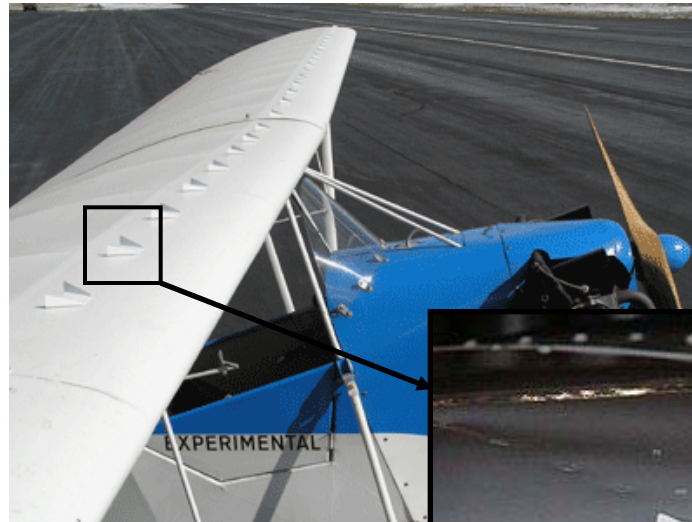
# OUTLINE

1. INTRODUCTION
2. COMPUTATIONAL SET UP
3. RESULTS
4. CONCLUSIONS
5. FUTURE WORK



# Introduction

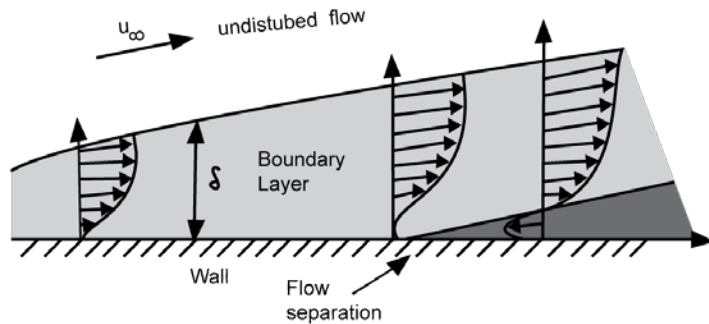
## Applied aerodynamics on aircraft wings



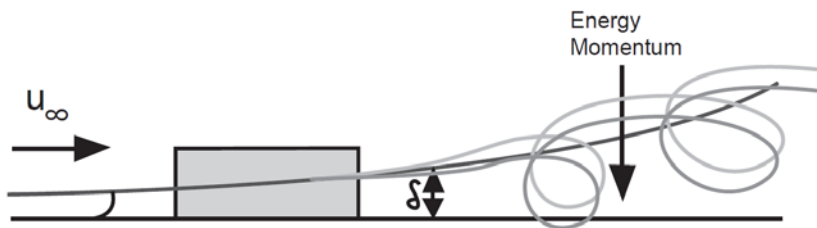
Source: Vortex generators on the wing of an airplane at the Air Force Museum of the German Federal Armed Forces in Berlin. Image credit: Wikimedia Commons  
<http://phys.org/news/2012-09-scientists-purpose-vortex.html#iCp>



# What is a VG? How does it work?



**Figure 1:** Evolution of boundary layer velocity profiles with adverse pressure gradient.



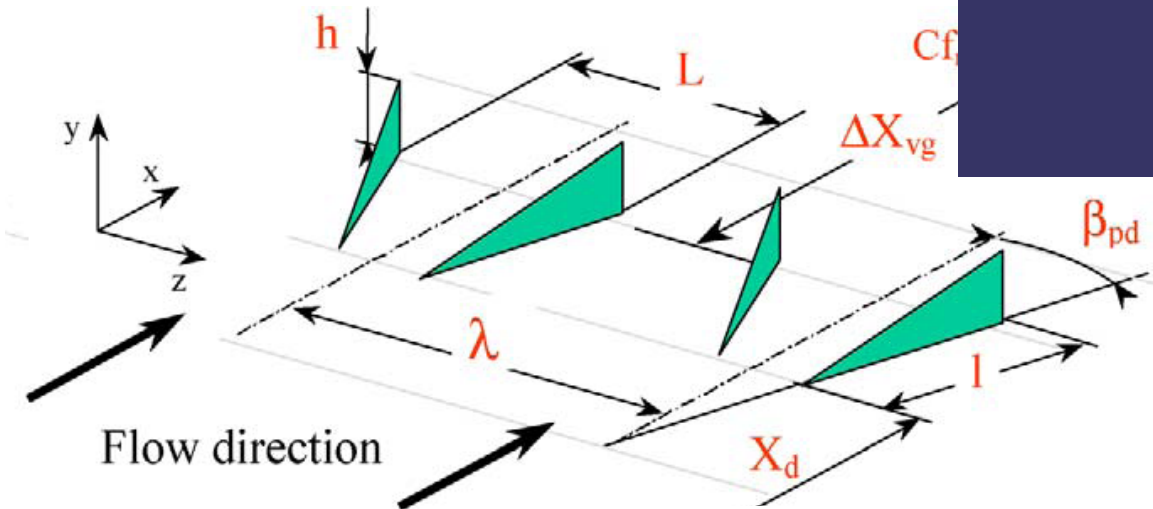
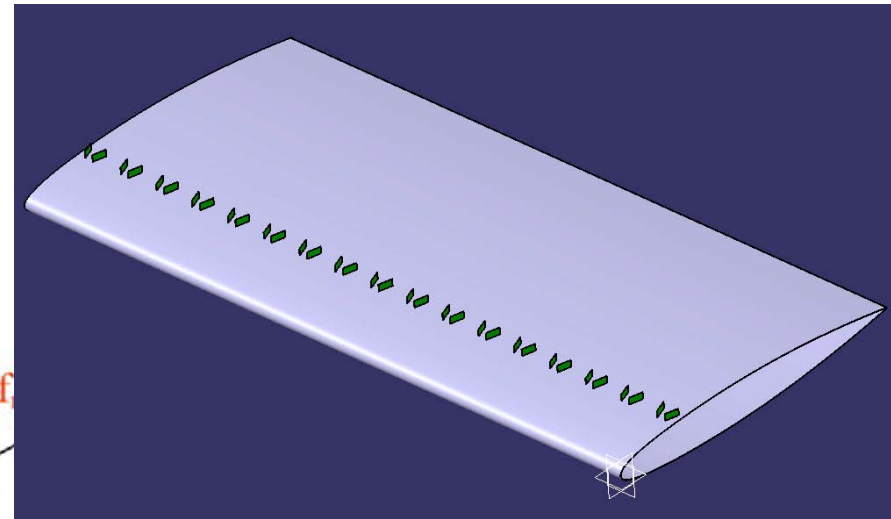
**Figure 2:** Boundary layer motion alteration by a rectangular VG.

These passive devices are used for flow control:

- Modifying the boundary layer motion.
- Generation of longitudinal vortices.
- Overturn of the BL flow via large scale motions.
- Bringing high momentum fluid down into the near wall region of the boundary layer.
- In short: separation of the flow is delayed.

# VGs on Airfoils

- GEOMETRY: triangular or rectangular vanes.
- Dimensioned : to the local boundary layer thickness.
- Lay-out: in cascades in groups of two.



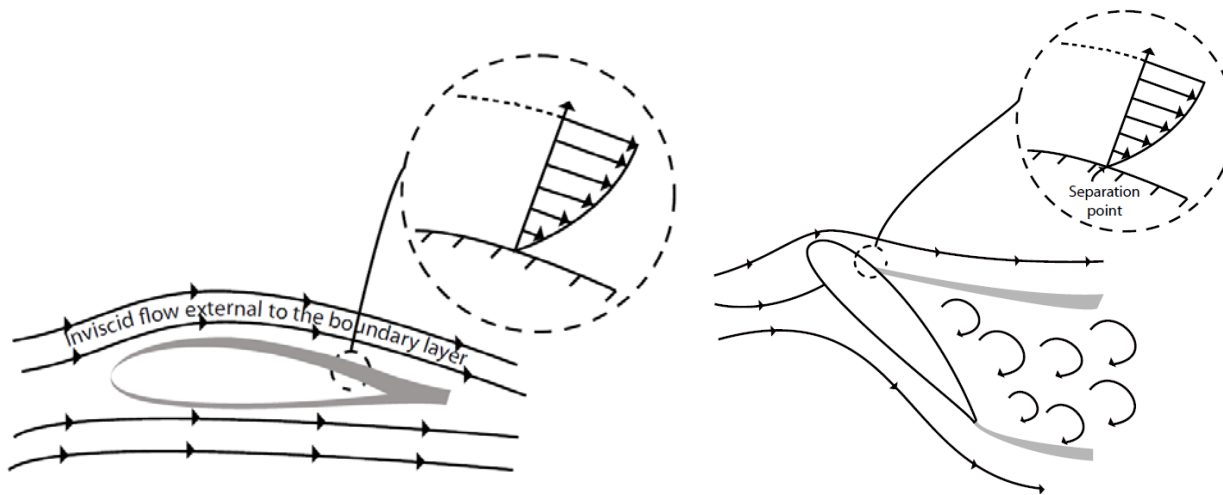
Ref.: G. Godard , M.  
Stanislas 2005

**Figure 3:** Counter rotating passive device configuration.



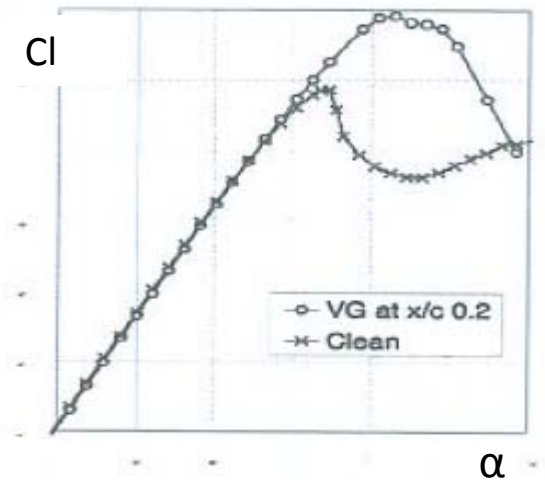
# VGs on Airfoils

- Main functionality:
  - to delay or prevent separation of the flow.



**Figure 4:** (a) Flow across an airfoil. (b) Separated flow over the top surface of an airfoil)

SOURCE: J.D. Anderson Jr., Brief History of the Early Development of Theoretical and Exp. Fluid Dynamics Wiley & Sons 2010

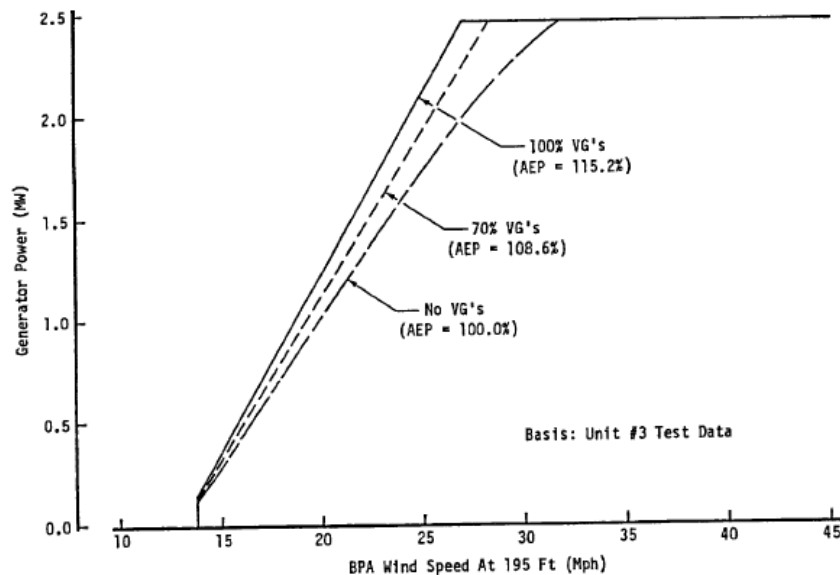


**Figure 5:** effect of vortex generators on the performance of DU 97-W-300.

Ref.: van Rooij R. P. J. O. M. and Timmer W A "Roughness Sensitivity Considerations for Thick Rotor Blade Airfoils". AIAA-paper 2003-0350.

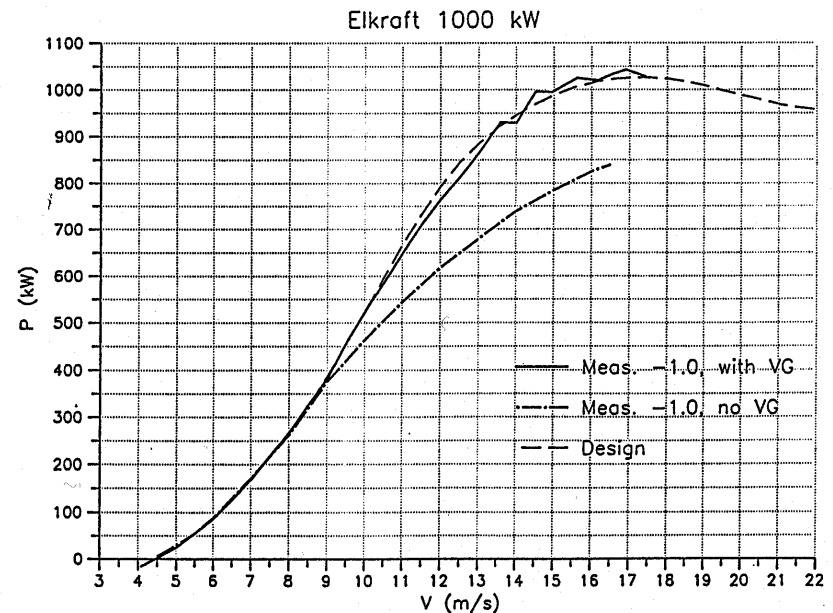
# VGs on Wind Turbines

Increased wind turbine performance from implementing VGs on the blades has also been confirmed through various field tests.



**Figure 6 (a):** Effects of VGs on a 2.5 MW wind turbine performance.

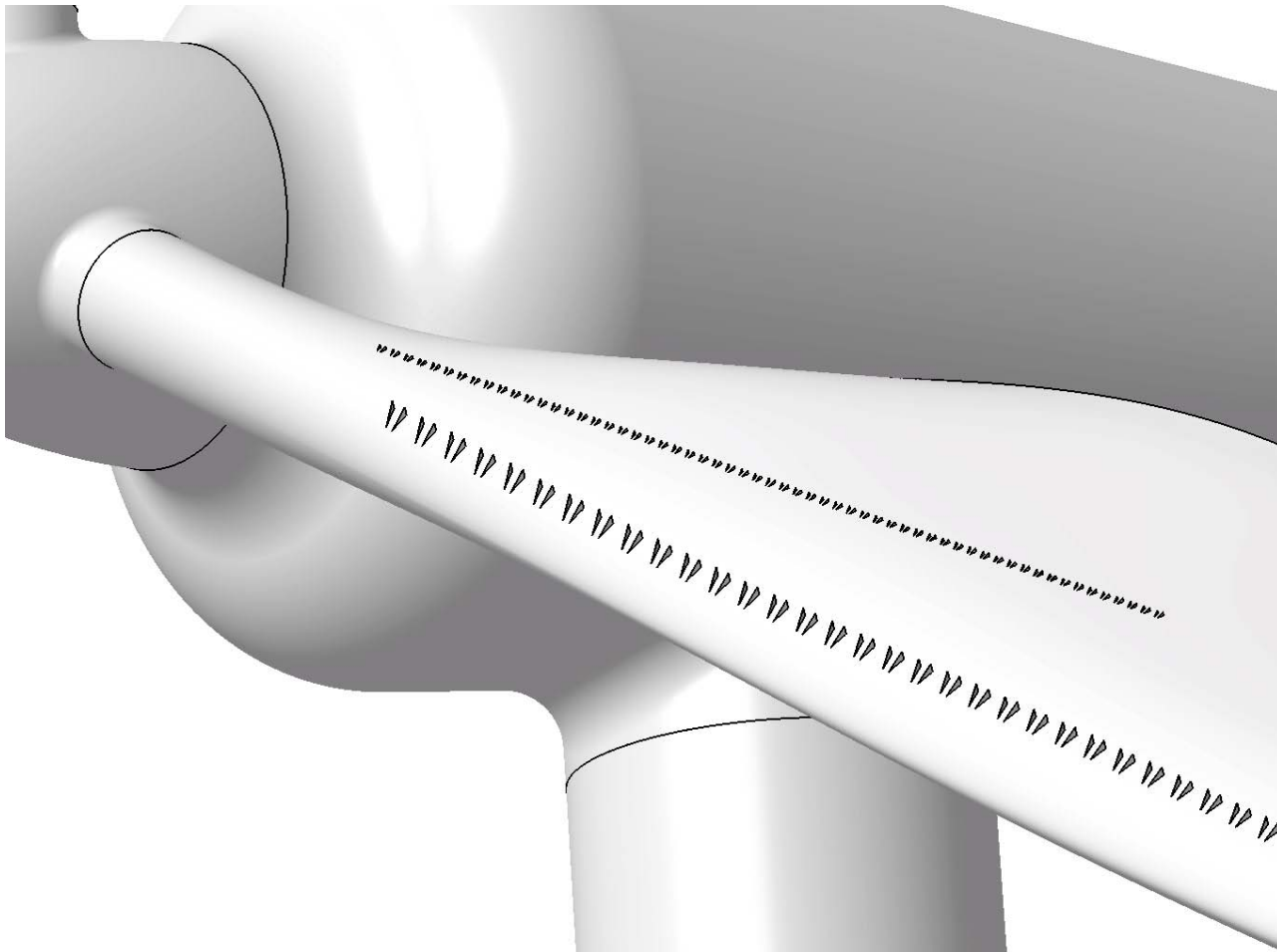
Ref.: Miller, G.E., "Comparative Performance Tests on the Mod-2 2.5 MW Wind Turbine With and Without Vortex Generators," NASA TM N95-27978, Presented at the DOE/NASA Workshop on Horizontal Axis Wind Turbine Technology, May 8-10, 1984, Cleveland, OH.



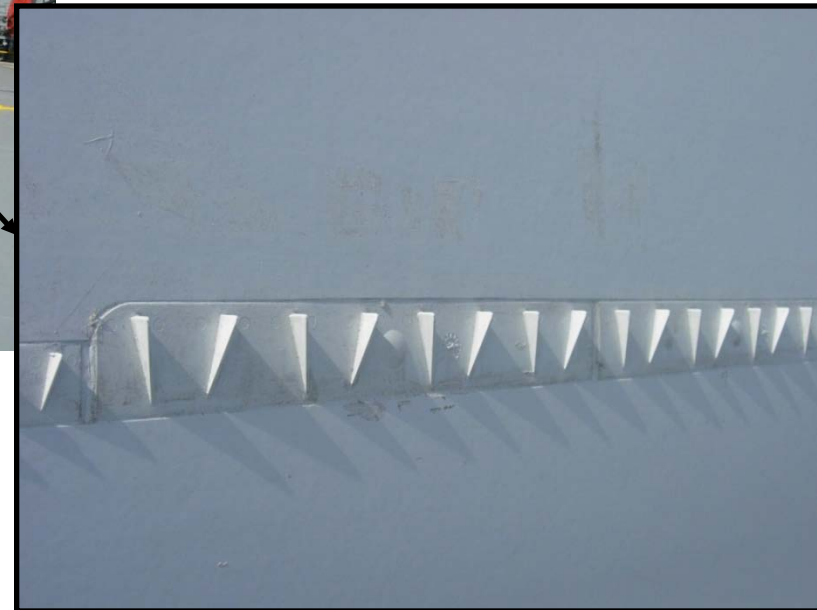
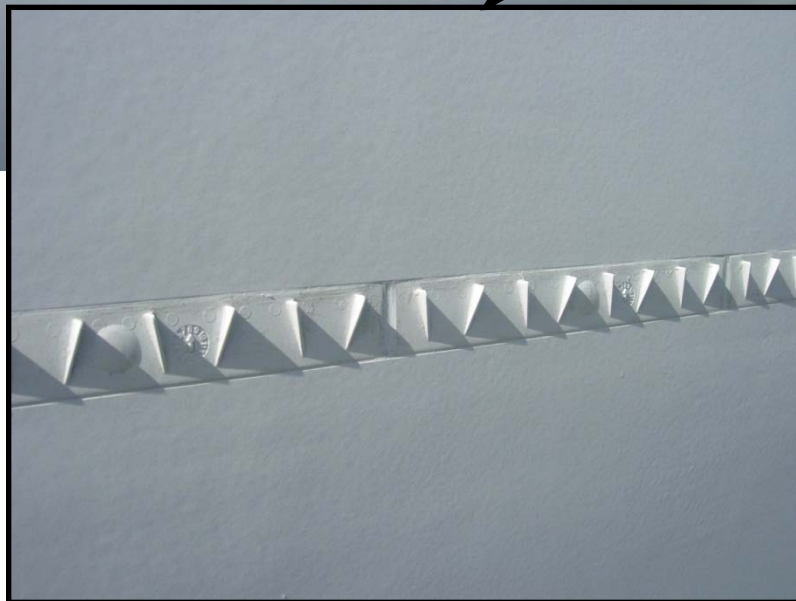
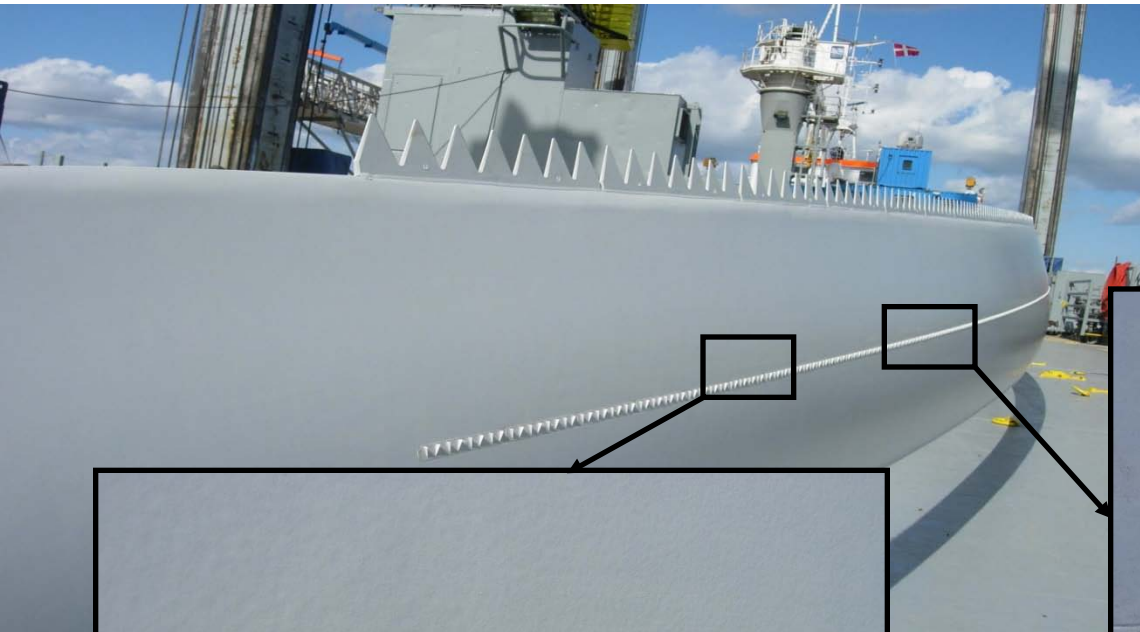
**Figure 6 (b):** Effects of VGs on a 1 MW wind turbine performance.

Ref.: S. Øye, *The effect of Vortex Generators on the performance of the ELKRAFT 1000 kW Turbine*, 9<sup>th</sup> IEA Symp. On Aerodynamics of Wind Turbines, 1995.

# VGs on Wind Turbines

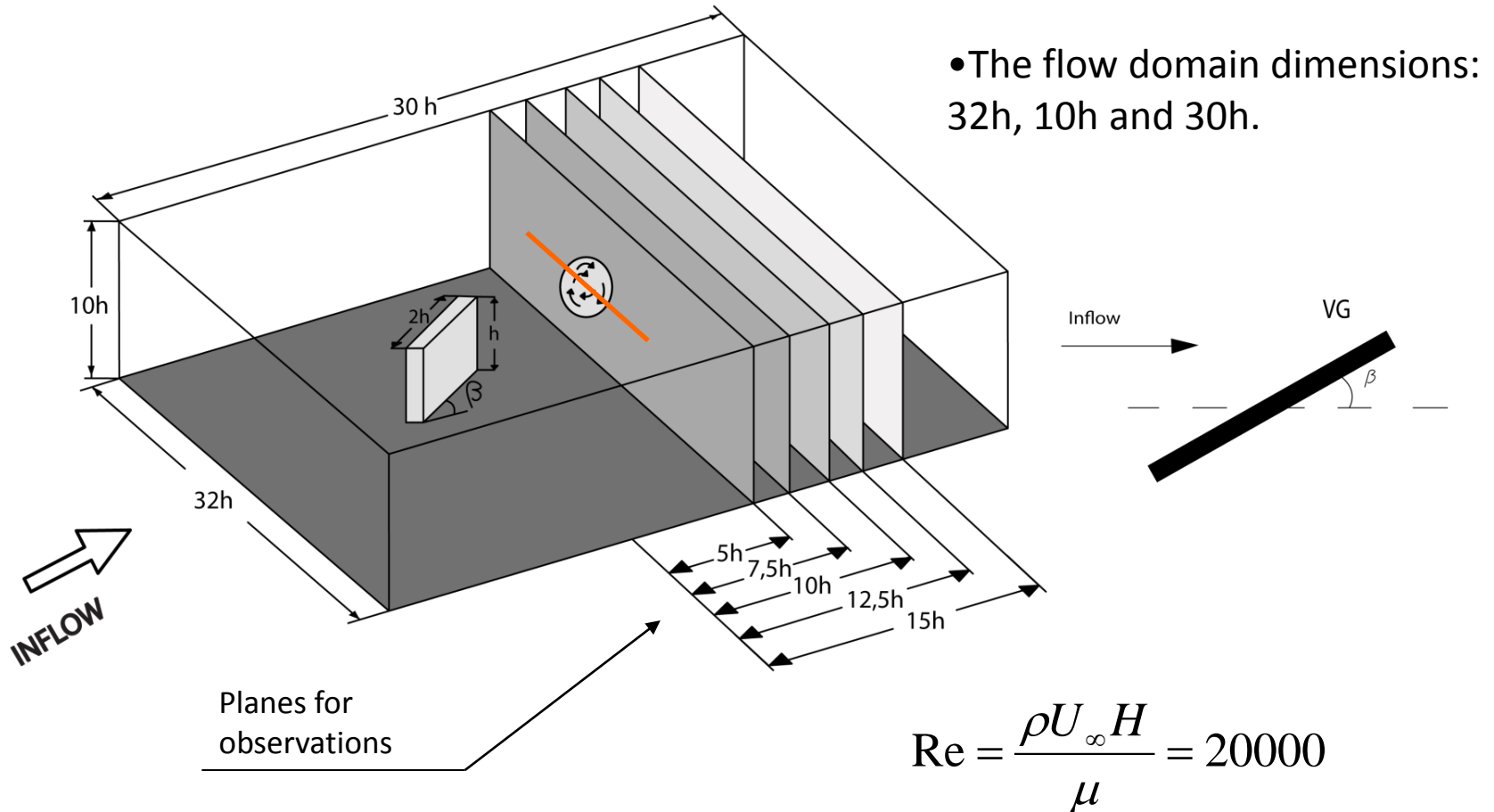


# VGs on Wind Turbines



SOURCE: pictures were taken by the author in EWEA Conference 2012, Copenhagen.

# Computational Set Up

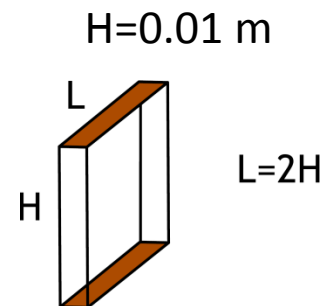


**Figure 7:** Computational domain and plane location where the measurements were conducted

# Computational Set Up

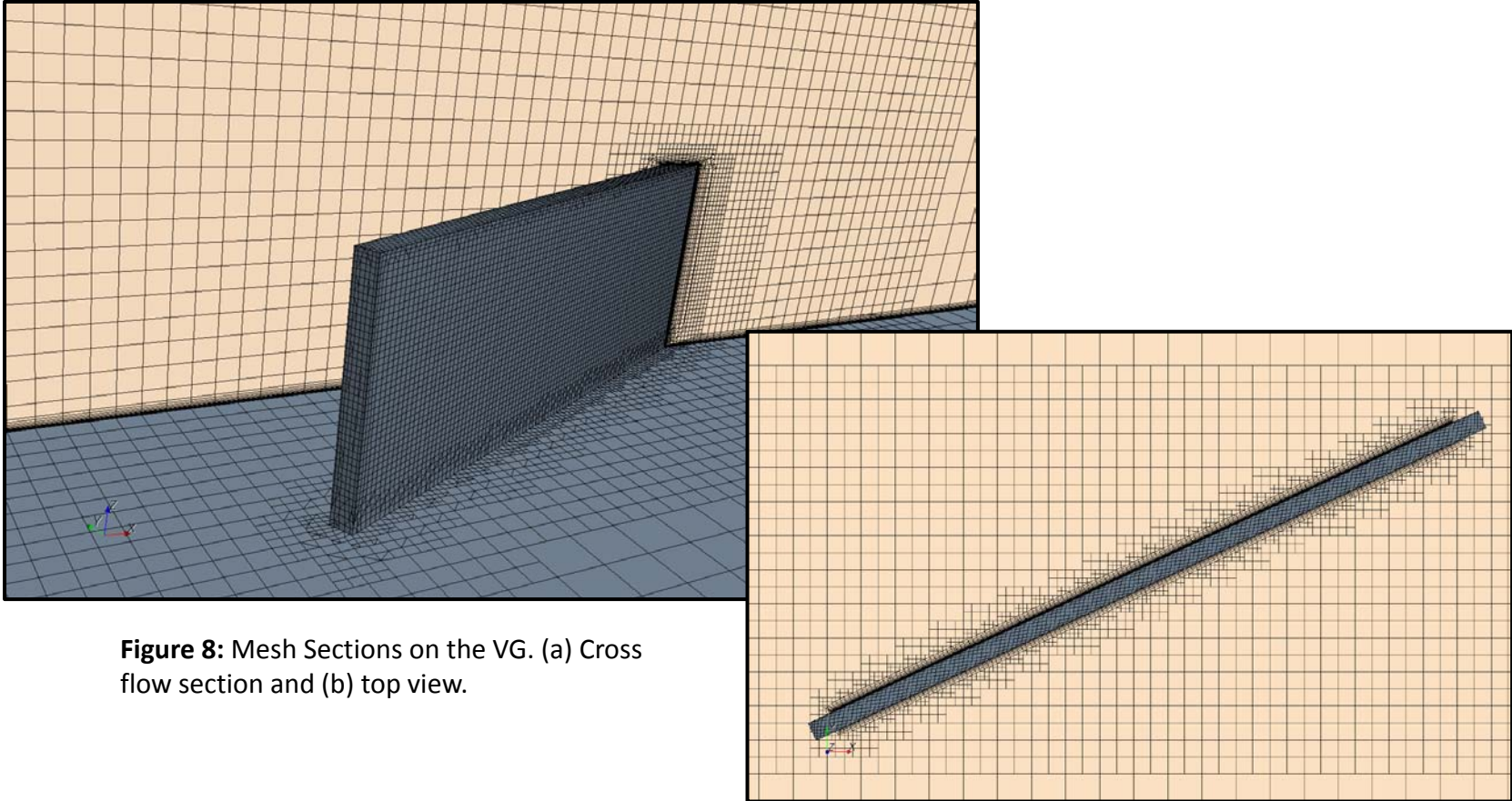
- **Unsteady state** computations have been carried.
- CFD computations: EllipSys3D code. RANS equations.
- The convective terms are discretized utilising the third order Quadratic Upstream Interpolation for Convective Kinematics (QUICK).
- ***k- $\omega$  SST*** (Shear Stress Transport)

$$\text{Re} = \frac{\rho U_{\infty} H}{\mu} = 20000$$



# Mesh

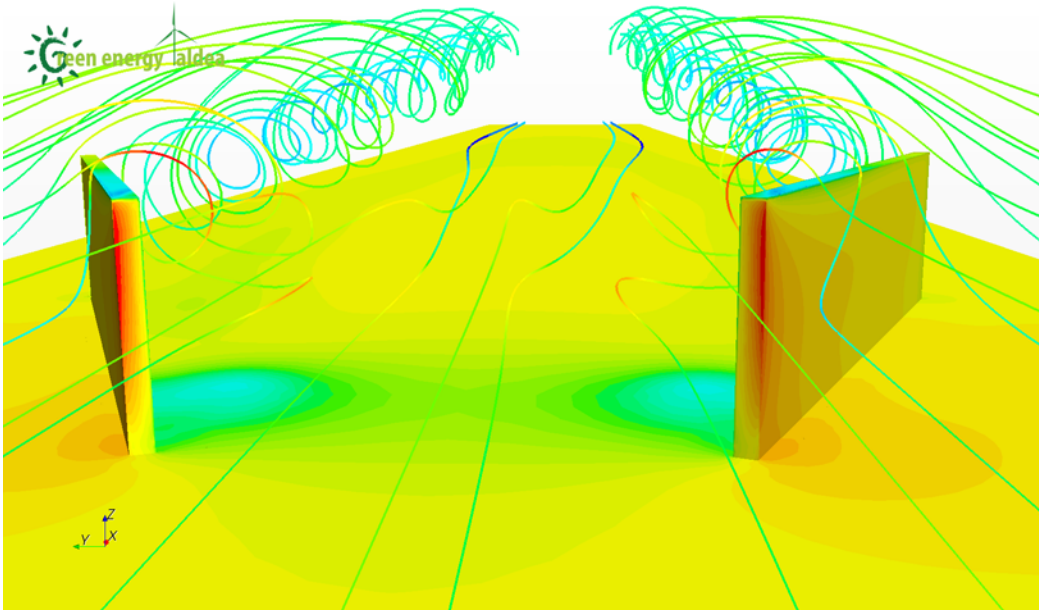
- Block structured mesh ( $2 \times 10^6$  cells)
  - Around the VG geometry:  $7 \times 10^5$  cells.
- Downstream the VG:  $4 \times 10^5$  cells.



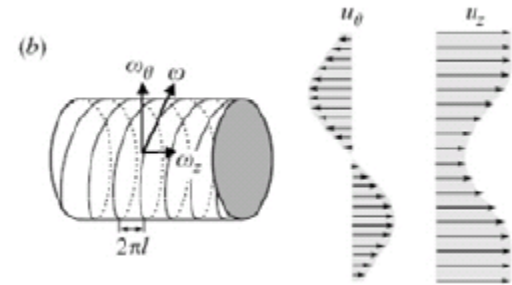
**Figure 8:** Mesh Sections on the VG. (a) Cross flow section and (b) top view.

# Analytical model

- The axial,  $u_z$ , and rotational,  $u_\theta$ , velocities are linearly related:



$$u_z = u_0 - r u_\theta / l$$



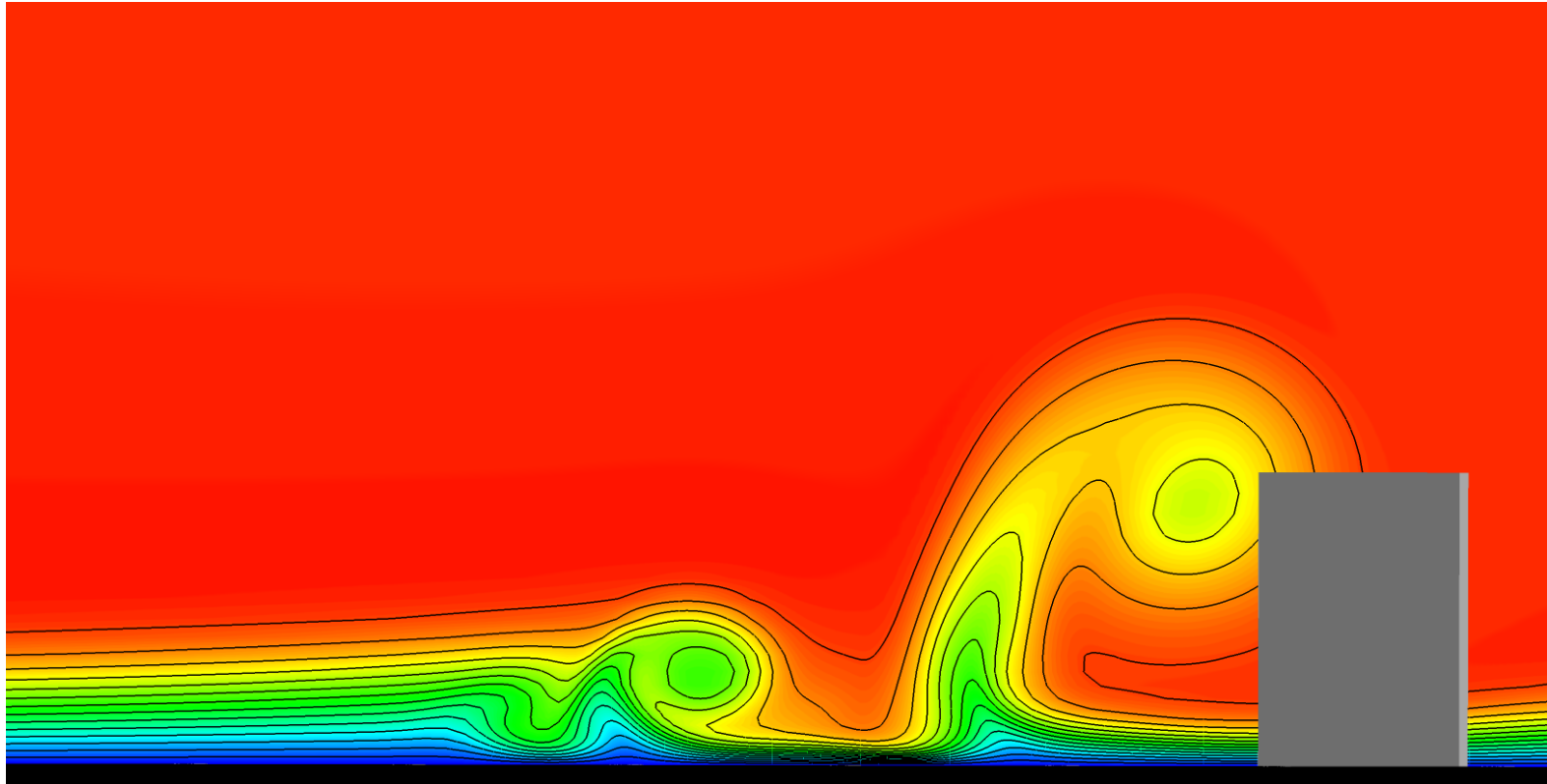
Together with the Batchelor vortex model

$$u_\theta(r, \theta, z) = \frac{\Gamma(z)}{2\pi r} \left[ 1 - \exp\left(-\frac{r^2}{\varepsilon^2(\theta, z)}\right) \right]; \quad u_z(r, \theta, z) = u_0(z) - \frac{\Gamma(z)}{2\pi l(\theta, z)} \left[ 1 - \exp\left(-\frac{r^2}{\varepsilon^2(\theta, z)}\right) \right]$$

four parameters:  $\varepsilon(\theta, z)$ , circulation  $\Gamma(z)$ ,  $u_0(z)$  and  $l(\theta, z)$ ,



# Axial Velocity Fields

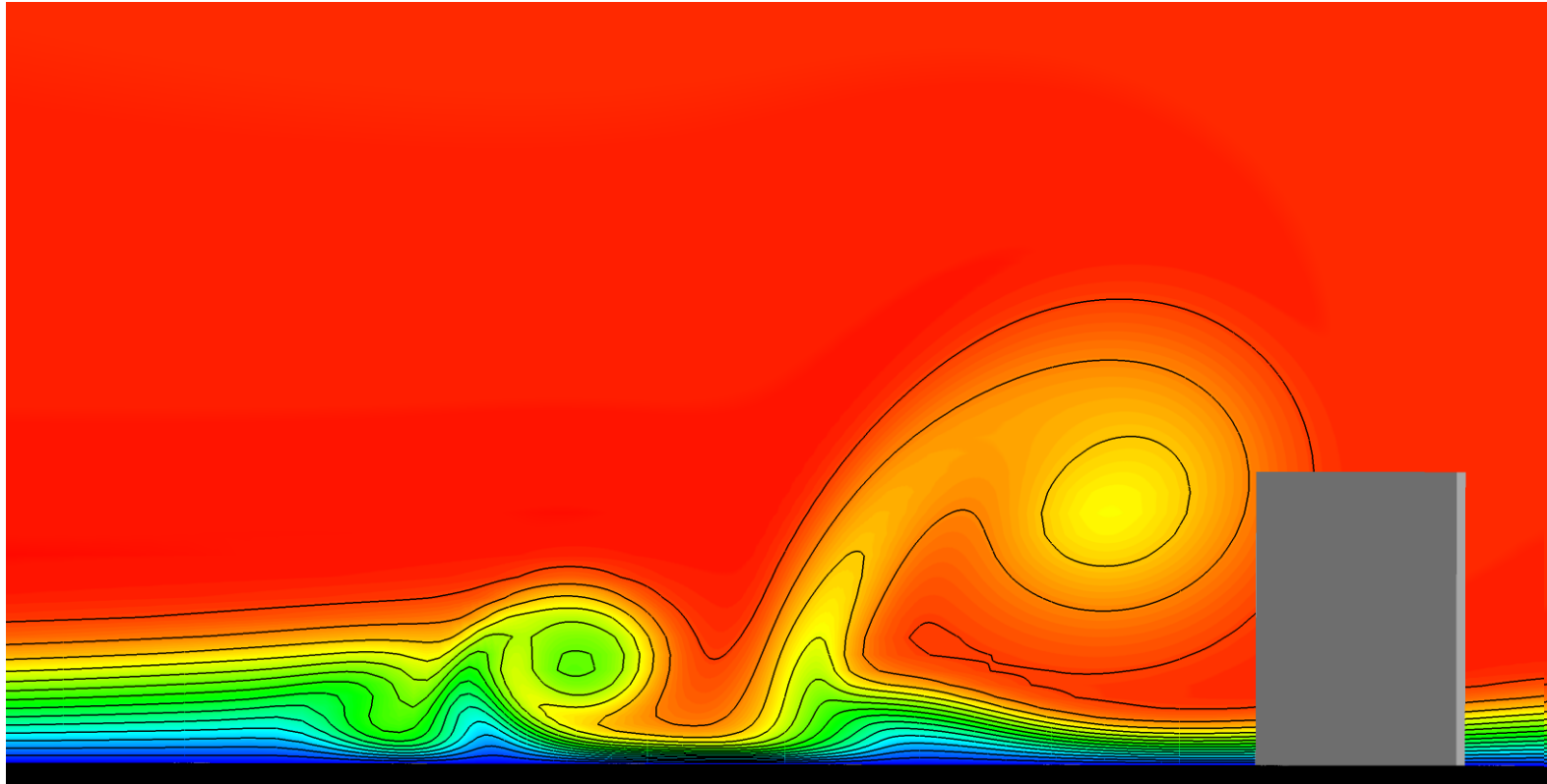


$$x/h = 5$$

**Figure 9:** Axial velocity fields at five plane positions:  $z/h = 5-15$ .



# Axial Velocity Fields

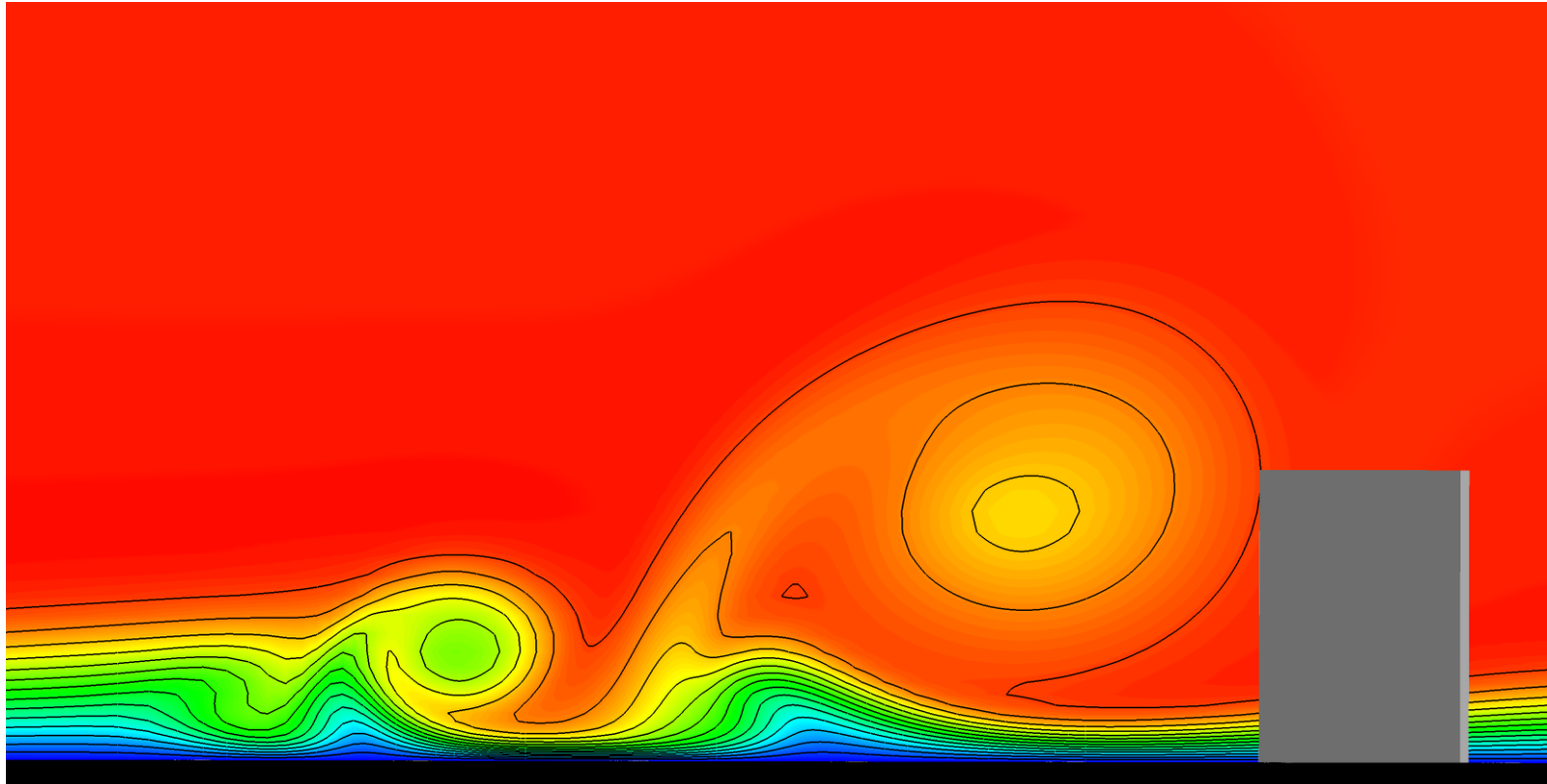


$$z/h = 7.5$$

**Figure 9:** Axial velocity fields at five plane positions:  $z/h = 5-15$ .



# Axial Velocity Fields

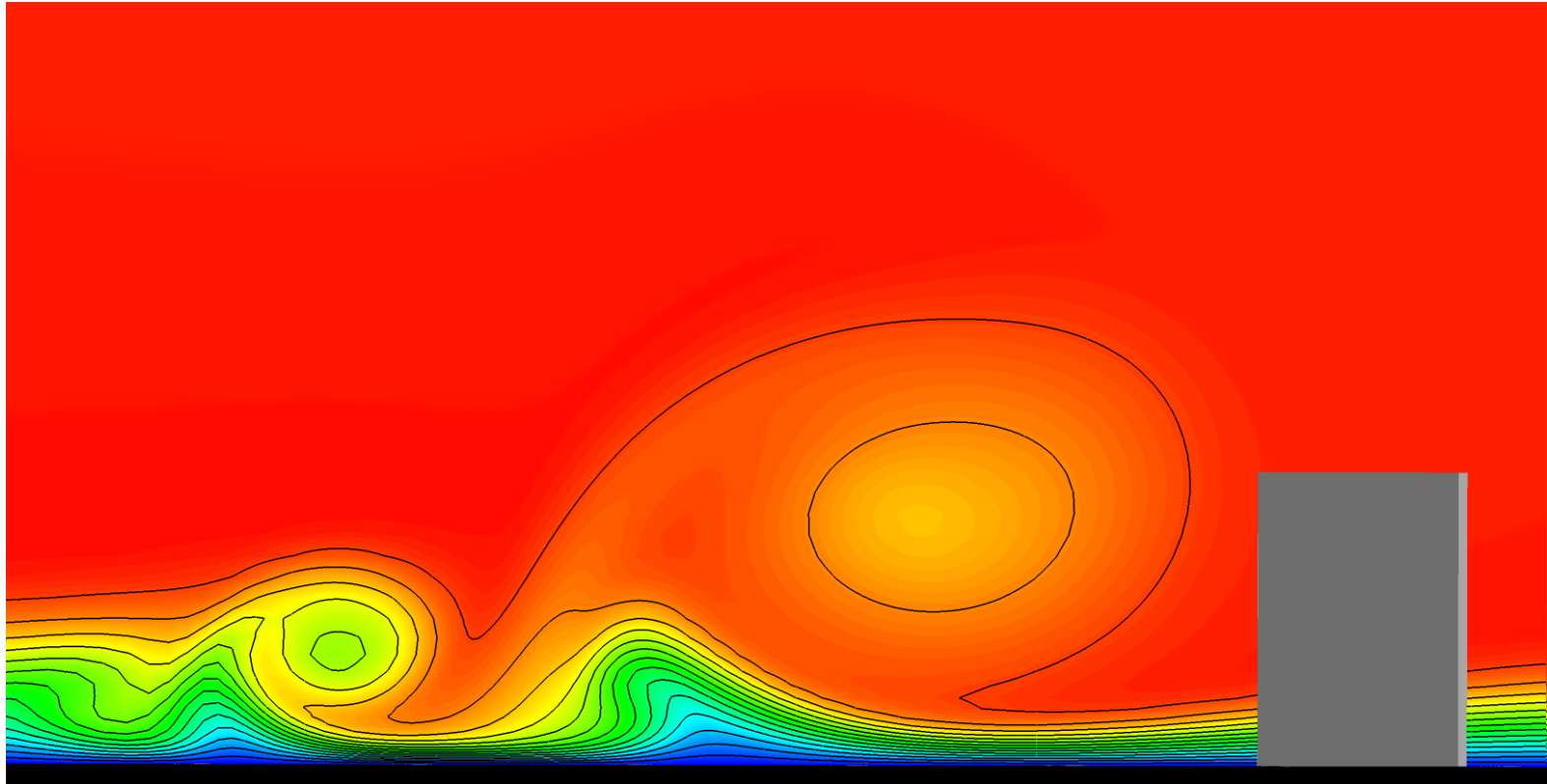


$$x/h = 10$$

**Figure 9:** Axial velocity fields at five plane positions:  $z/h = 5-15$ .



# Axial Velocity Fields

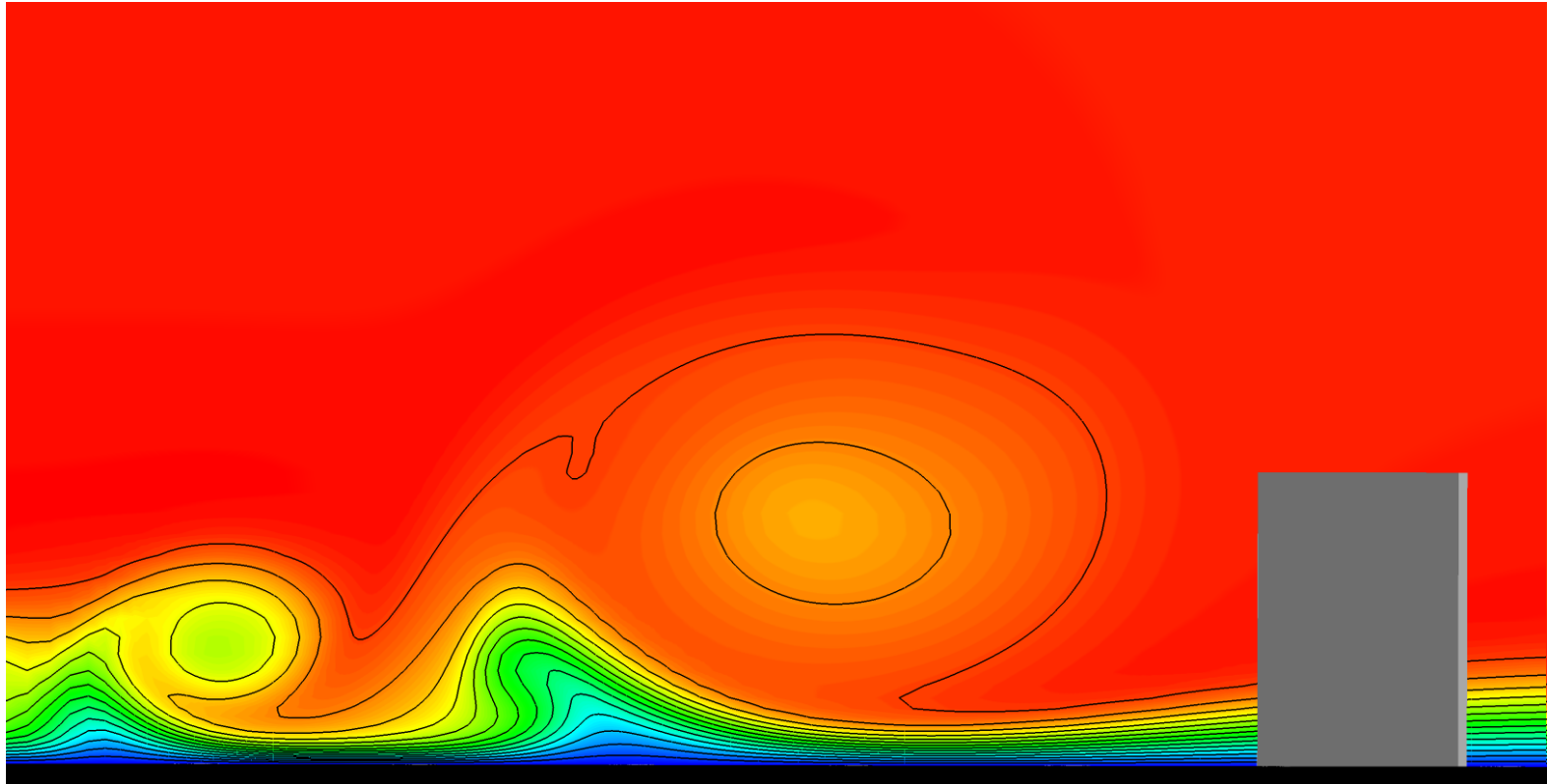


$$x/h = 12.5$$

**Figure 9:** Axial velocity fields at five plane positions:  $z/h = 5-15$ .



# Axial Velocity Fields

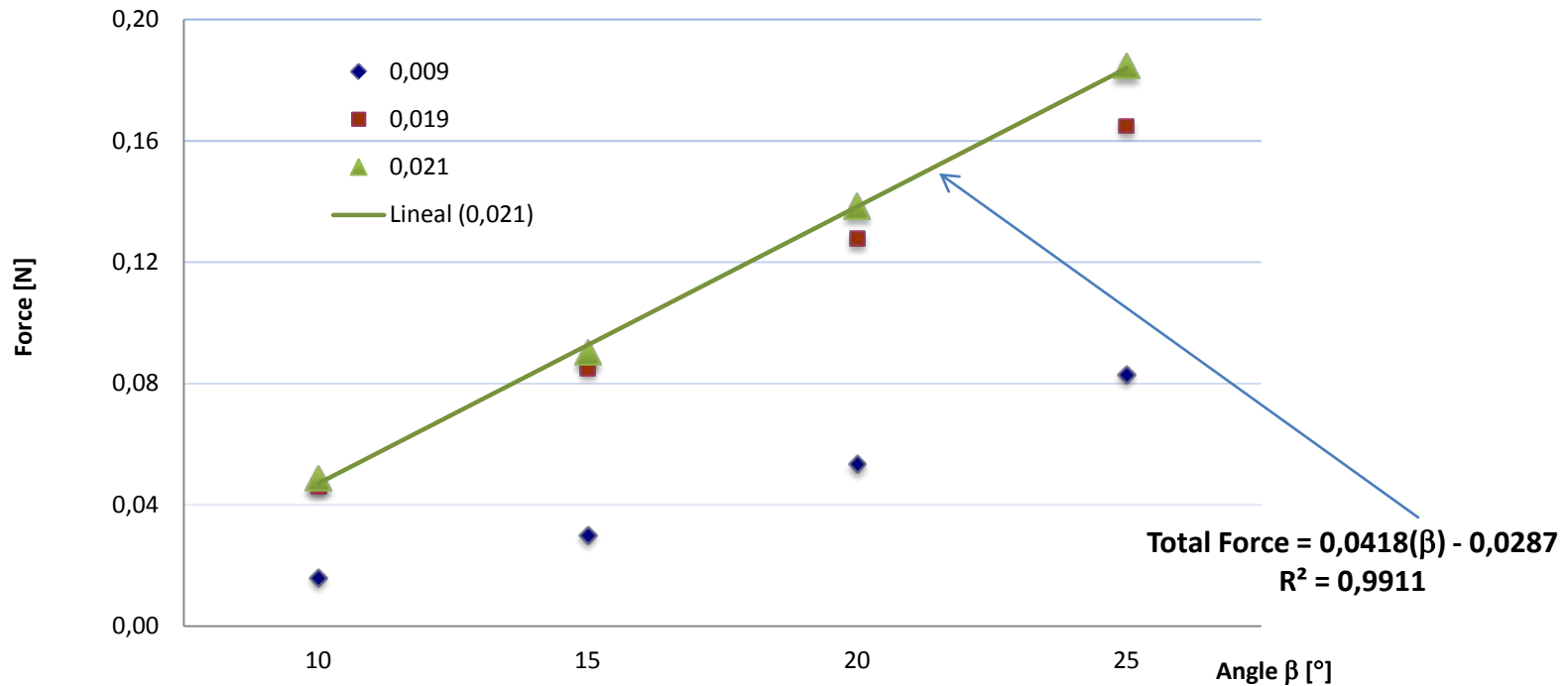


$$x/h = 15$$

**Figure 9:** Axial velocity fields at five plane positions:  $z/h = 5-15$ .



# FORCES PLOT



Angle [°]	Force x [N]	Force Y [N]	Total Force [N]
5	0,009	0,019	0,021
10	0,016	0,046	0,049
15	0,030	0,085	0,090
20	0,053	0,128	0,139
25	0,083	0,165	0,185

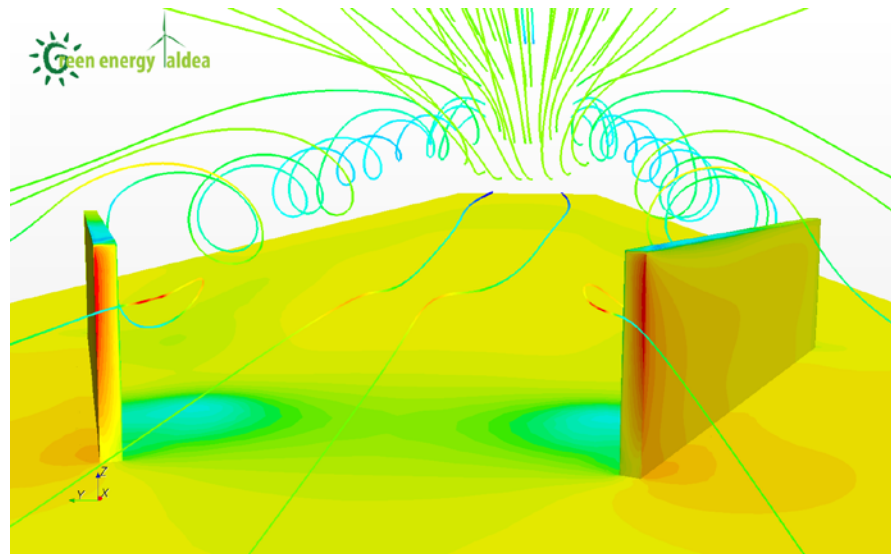
# Conclusions

- The main vortex generated by the VG possesses helical symmetry and self-similar behavior for both the axial and azimuthal velocity profiles. It has been proven based on five plane positions  $z/h=5-15$  downstream of the trailing edge of the VG and with  $\beta=20^\circ$  of the vane to the incoming flow.
- From the point of view of self-similarity, computational simulations are able to reproduce the physics of the vortex generated by a rectangular VG with considerable reliability.



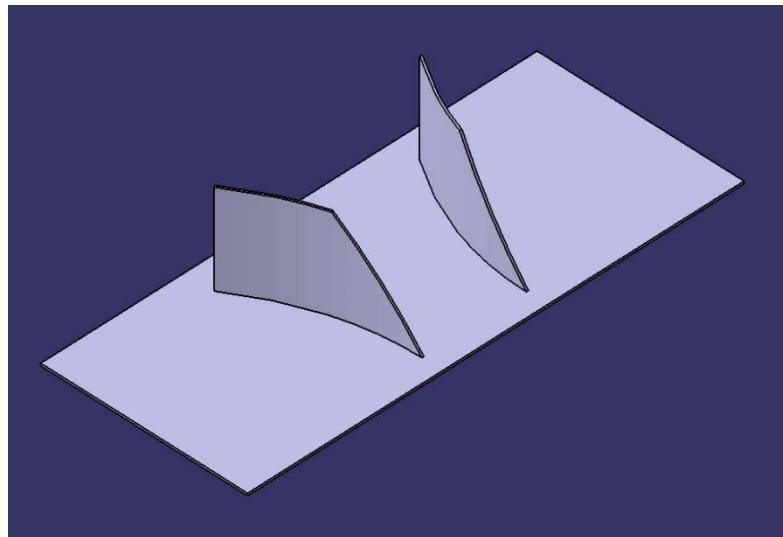
# Future Work

- Additional work:
  - Comparison with wind tunnel experimental data.
  - Computations with Different VG geometries.



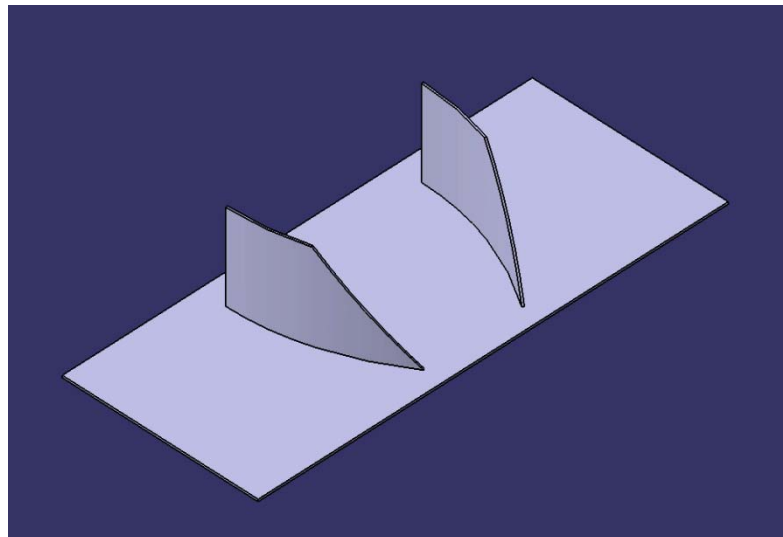
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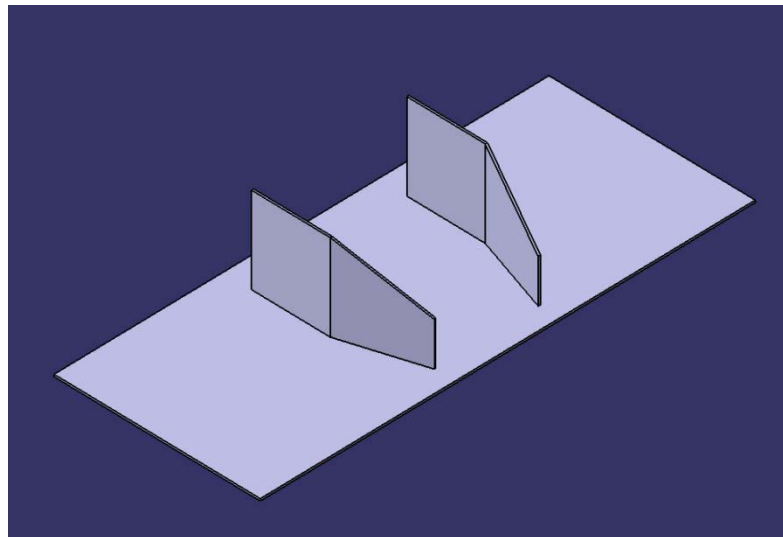
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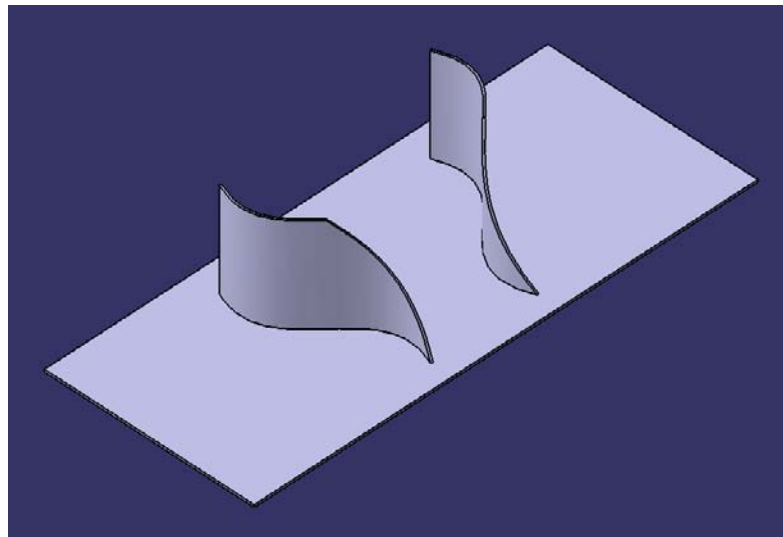
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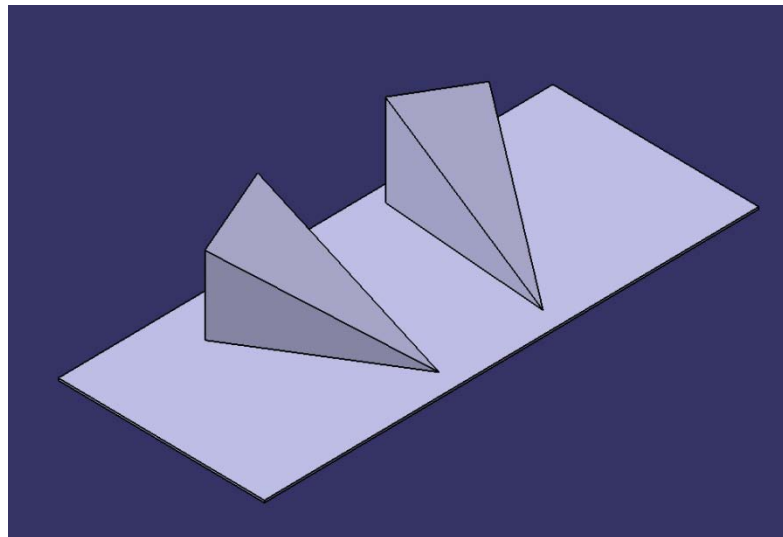
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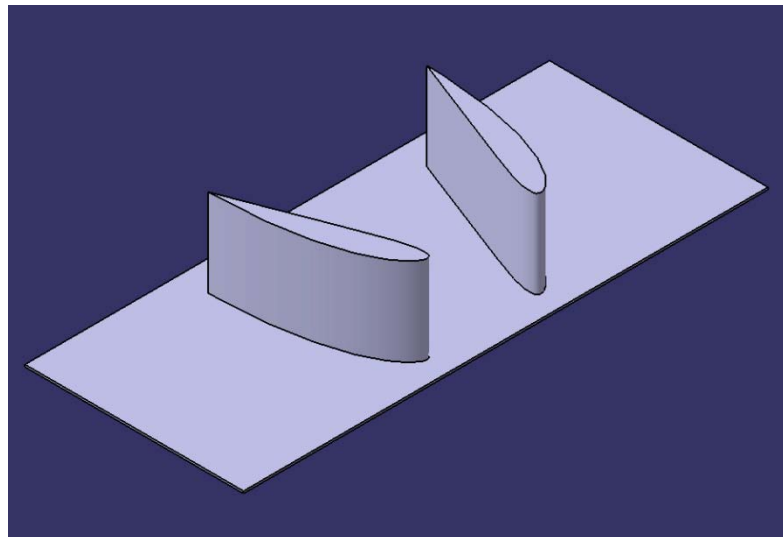
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***Thank you very much for your attention!***

***Eskerrik asko zuen arretagatik!***

***¡Muchas Gracias por vuestra atención!***

